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# Jet and Rocket Propulsion

## AE4451

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### LECTURE 6

# Overview

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what we saw last time:

- mixtures of perfect gases
  - calculations: summation over constituents and averaged properties

today:

- chemical equilibrium thermodynamics

# Chemical equilibrium thermodynamics

- up to this point, we've considered "frozen" flows:
  - no changes to chemical composition
- chemically-reacting flows are relevant to several propulsion systems
  - e.g. rocket combustion chambers

some helpful assumptions are generally made:

- (a) individual gases can be treated as perfect
- (b) generally, chemically processes occur between states that are in equilibrium

- chemically-reacting flows are relevant to several propulsion systems
  - e.g. rocket combustion chambers

# Chemical transformations

- determining the heat of reaction

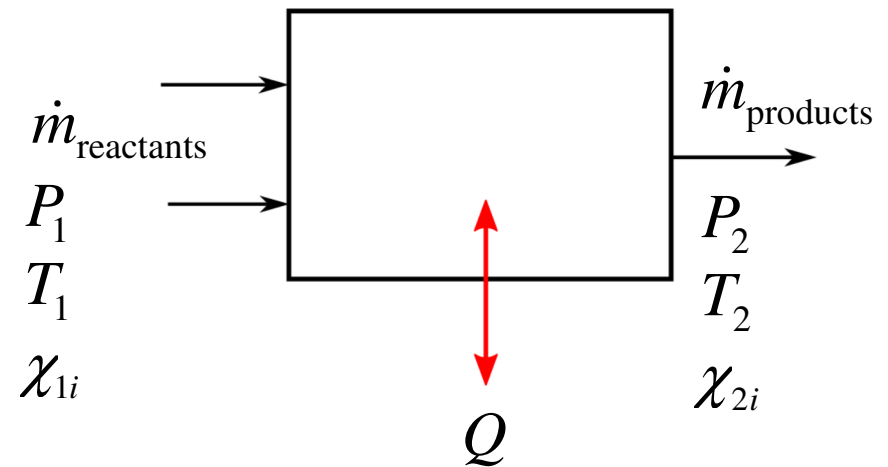
let's consider a steady-flow process + no work

$$Q = \Delta H \quad \text{heat transfer of the fluid through the control volume = change in enthalpy}$$

for one mole of product

$$Q = Q_r = H_{\text{products}} - H_{\text{reactants}}$$

$T_f$  temperature at which  $Q_r$  is measured



# Chemical transformations

- General approach
  1. apply mass conservation
    - atom balances or balancing stoichiometric reactions  $\alpha A + \beta B + \dots \rightarrow \gamma C + \delta D + \dots$
  2. apply energy conservation
    - defining chemical “energy” or enthalpy of formation
  3. apply entropy conservation (2<sup>nd</sup> Law)
    - maximize entropy to find equilibrium

# Chemical energy

- in nonreacting thermodynamics we combined all different types of energy into **stagnation** or **total enthalpy**,

$$h_0 = h + u^2/2 \quad h_t$$

recall:

$$\dot{Q}_{in} - \dot{W}_{shaft} + \int_{CV} \rho \vec{f} \cdot \vec{u} dV - \int_{CS} p(\vec{u} - \vec{u}_{rel}) \cdot \hat{n} dA = \frac{d}{dt} \int_{CV} \rho e_o dV + \int_{CS} \rho h_o (\vec{u}_{rel} \cdot \hat{n}) dA$$

- value of  $h$  depends on our choice of reference state; does  $h(0 \text{ K}) = 0$  or  $h(298 \text{ K}) = 0$ ?
- for a chemically reacting system we want to find a way to add chemical energy

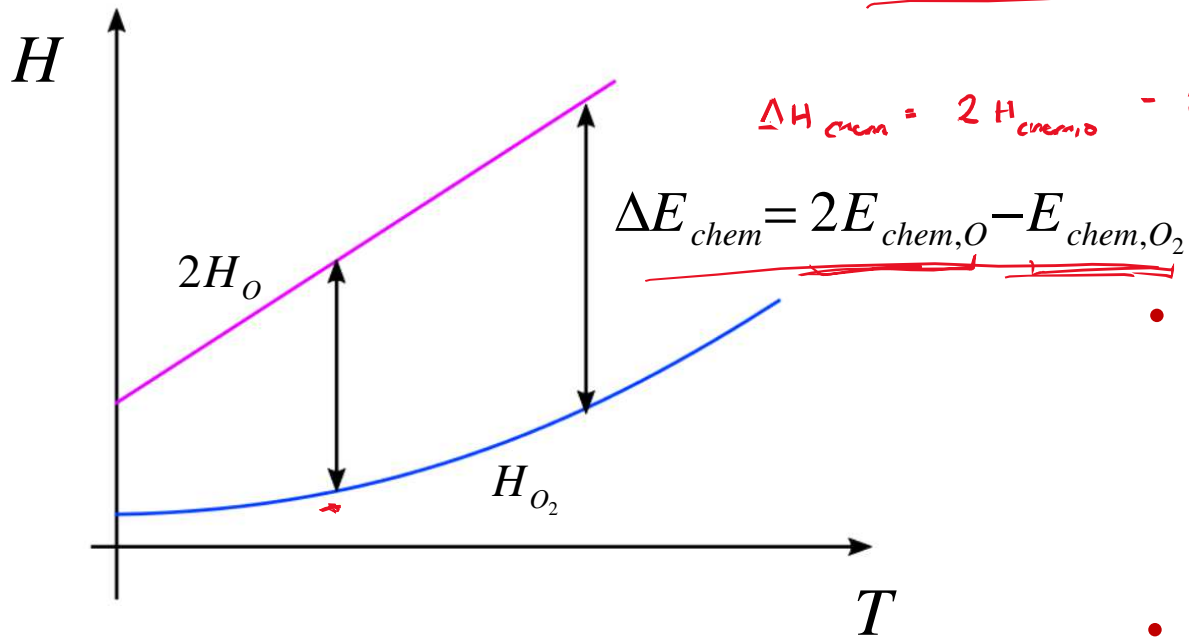
$$h_0 = h + u^2/2 + E_{chem}$$

- first, need to define a reference state where chemical energy is zero

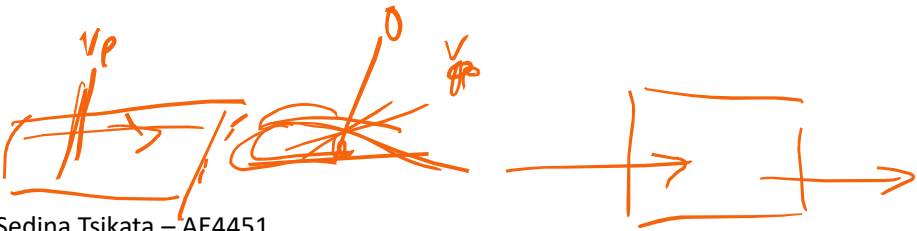
# Chemical energy

- enthalpy-temperature diagrams

single species example:  $O_2 \leftrightarrow 2O$



- is energy of O more or less than for  $O_2$ ?
- difference in energy between species is function of temperature

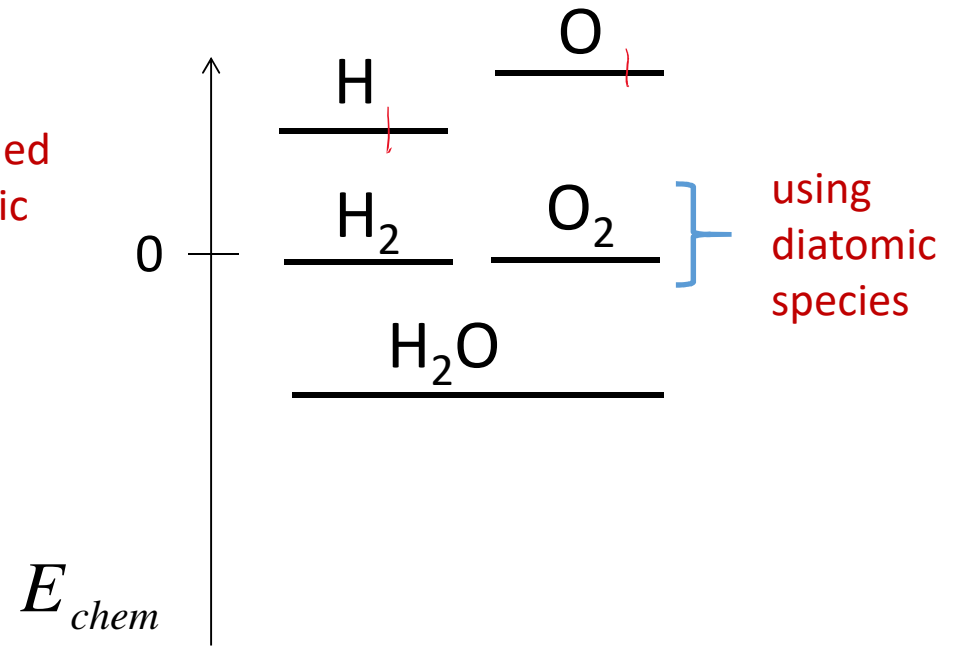
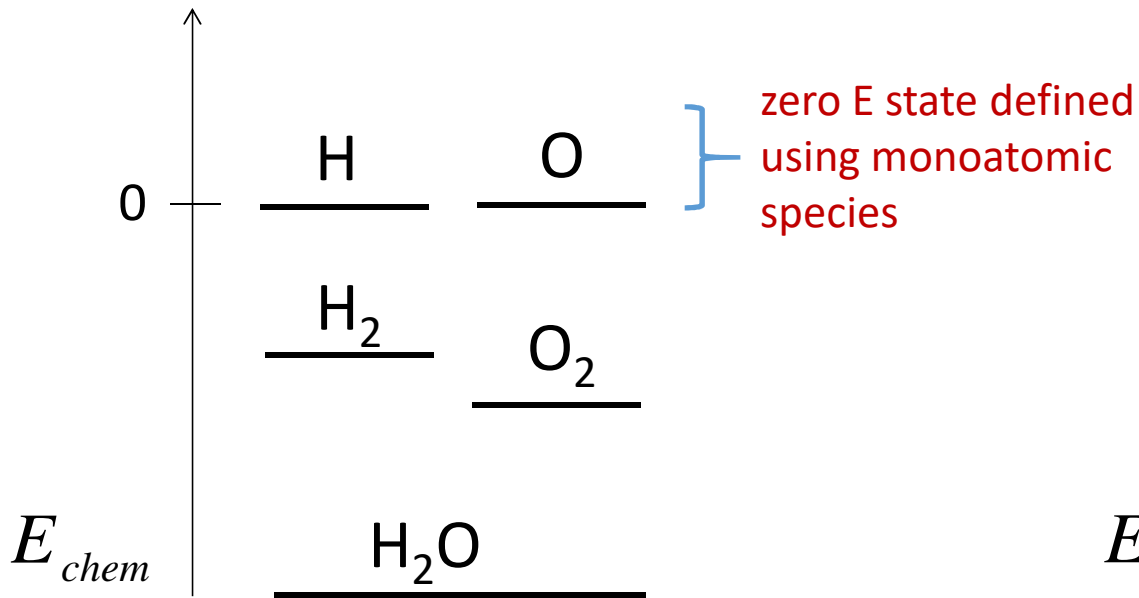


# Chemical energy

- enthalpy-temperature diagrams

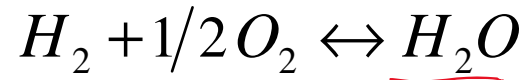
$H, O, H_2O, H_2, O_2$

multispecies example: how to define the zero energy state



# Heat of reaction

Q. What is the energy difference between the *products* and *reactants* if p,T constant? e.g.,



$$Q_R \text{ or } \underline{\Delta H_R} = \underbrace{E_{chem,H_2O}}_{\text{heat of reaction}} - \left( E_{chem,H_2} + 1/2 E_{chem,O_2} \right) = \underbrace{H_p}_{\text{products}} - \underbrace{H_r}_{\text{reactants}}$$

must be independent of the zero energy reference state we define

the transformation is characterized as

**exothermic** (giving off heat)  $\underline{\Delta H_R} < 0$

**endothermic** (requiring heat)  $\Delta H_R > 0$

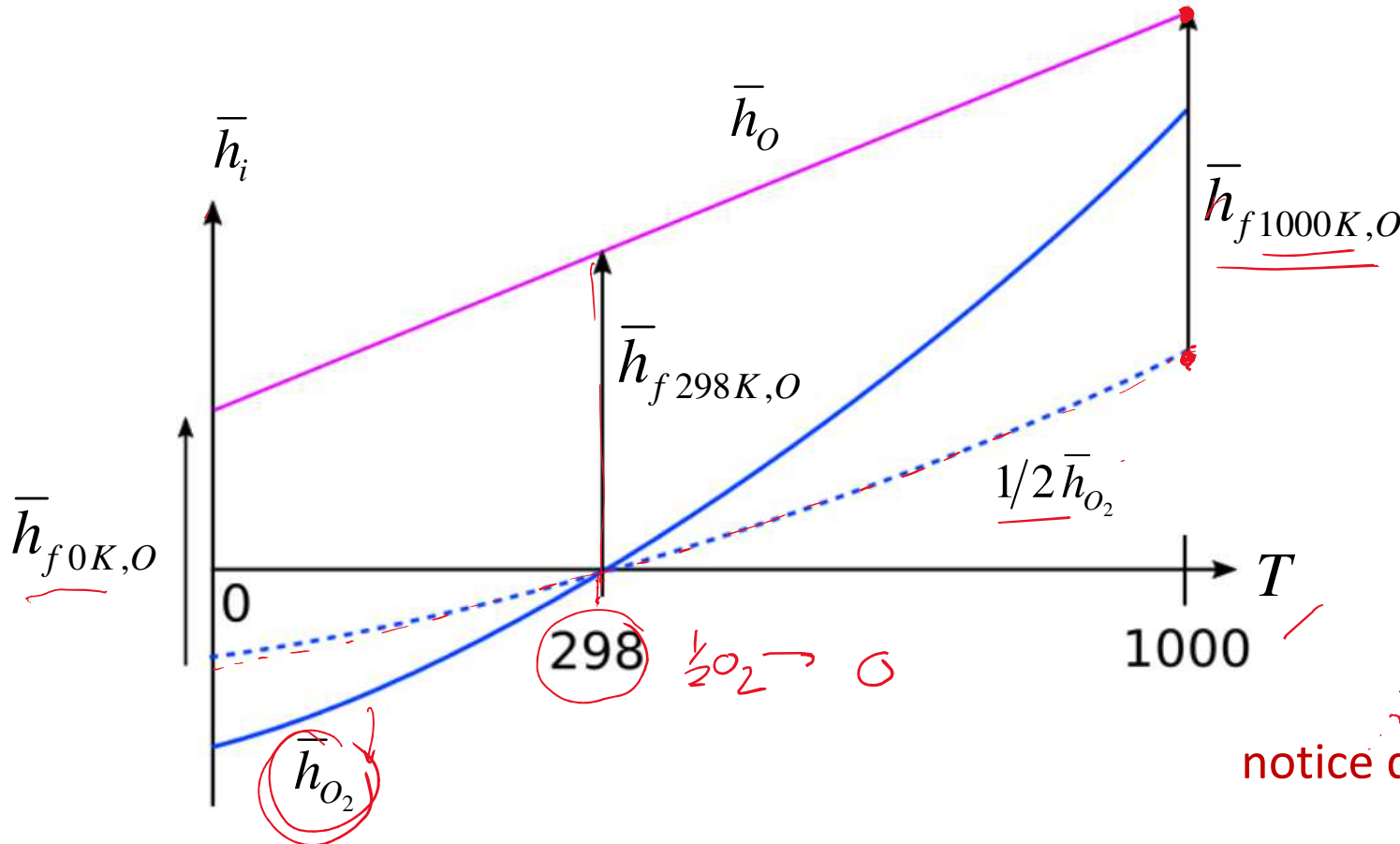
Heat of reaction = how much heat we would have to add to keep T constant (at fixed p) for specified composition change (reaction)

- we will often want to solve for the product state (p, T,  $\chi_i$ ) and determine the heat of a reaction



# Heat of formation: example

considering again  $O_2$  and  $O$ :  $1/2 O_2 \leftrightarrow O$



Q. what is enthalpy of formation of  $O_2$ ?

[kinetics.nist.gov/janaf](http://kinetics.nist.gov/janaf)  
0

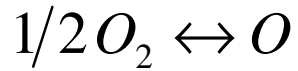
Q. what is enthalpy of formation of  $O$ ?

$$\Delta \bar{h}_{f,T,O}^o = \bar{h}_O(T) - 1/2 \bar{h}_{O_2}(T)$$

notice dependence on temperature

# Heat of formation: example

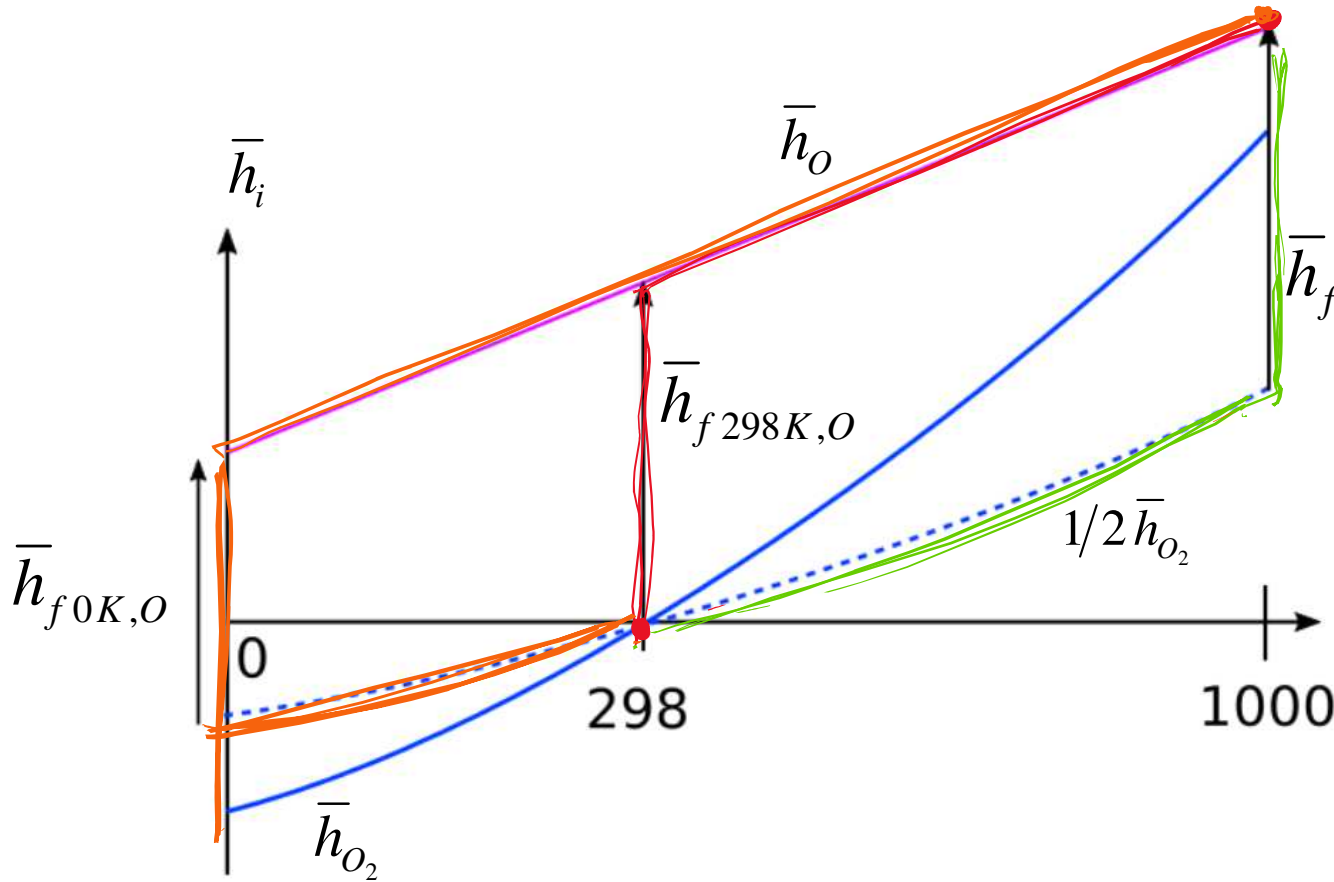
considering again O<sub>2</sub> and O:



Q. What is the enthalpy change going from ½ mole of O<sub>2</sub>@298K to O@ 1000K?

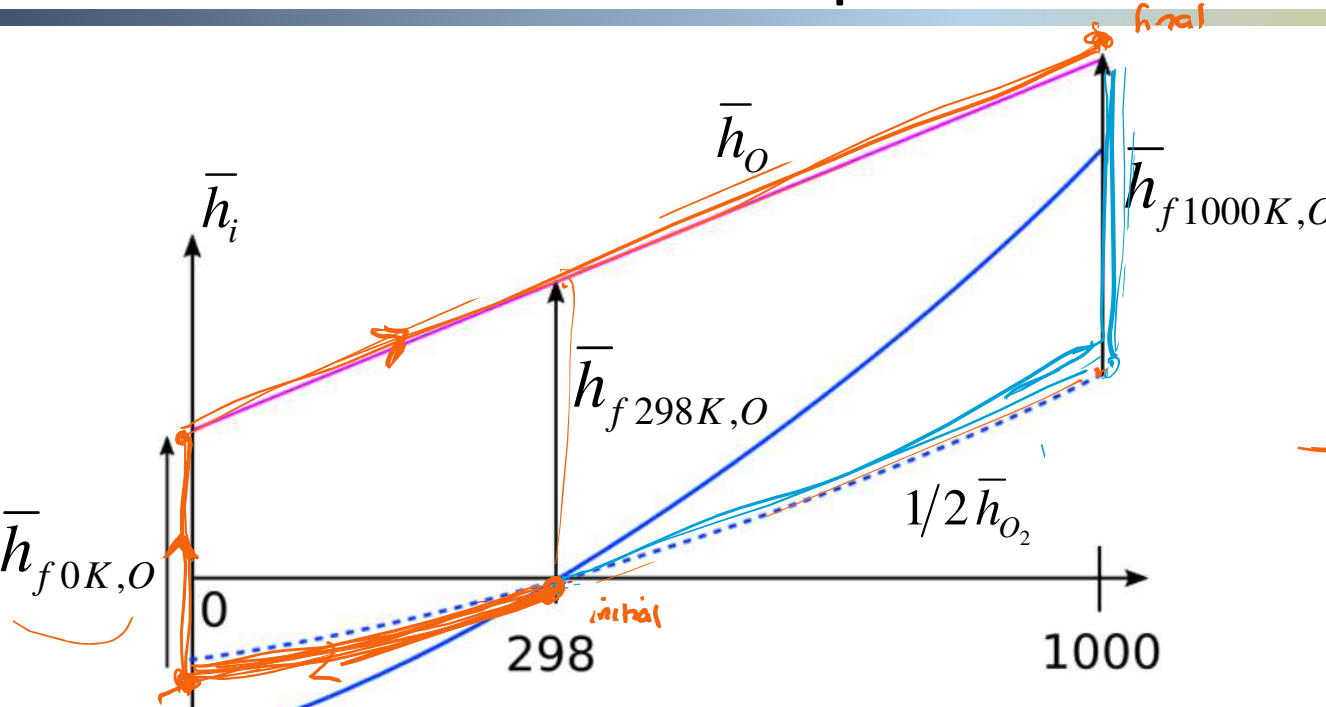
$$\Delta H = \underline{1\bar{h}_O(1000K)} - \underline{\frac{1}{2}\bar{h}_{O_2}(298K)}$$

how many pathways?



$\frac{1}{2}O_2 \rightarrow O$

# Heat of formation: example



Q. What is the enthalpy change going from  $\frac{1}{2}$  mole of  $O_2$  @ 298K to  $O$  @ 1000K?

$$\Delta H = 1\bar{h}_O(1000K) - 1/2\bar{h}_{O_2}(298K)$$

\* final - initial

$$\begin{aligned} \Delta H &= \left\{ \left[ \bar{h}_O(1000K) - \bar{h}_O(298K) \right] + \Delta \bar{h}_{f,298K,O}^o \right\} \\ &= \left\{ \bar{h}_O(1000K) - \bar{h}_O(1000K) \right\} + \Delta \bar{h}_{f,1000K,O}^o + \frac{1}{2} \left\{ \bar{h}_{O_2}(1000K) - \bar{h}_{O_2}(298K) \right\} \\ &= \left\{ \bar{h}_O(1000K) - \bar{h}_O(0K) \right\} + \Delta \bar{h}_{f,0K,O}^o + \frac{1}{2} \left\{ \bar{h}_{O_2}(0K) - \bar{h}_{O_2}(298K) \right\} \end{aligned}$$

# Heat of formation

So, generally, we can write the enthalpy as

$$\bar{h}_i(T) = \underbrace{(\bar{h}_T - \bar{h}_{T_{ref}})_i}_{\substack{\text{sensible} \\ h \text{ change}}} + \underbrace{\Delta \bar{h}_{f_{T_{ref},i}}^o}_{\text{chemical energy}} = \int_{T_{ref}}^T \bar{c}_{p,i} dT + \Delta \bar{h}_{f_{T_{ref},i}}^o$$

or, per unit mass:

$$h_i(T) = (h_T - h_{T_{ref}})_i + \Delta h_{f_{T_{ref},i}}^o = \int_{T_{ref}}^T c_{p,i} dT + \Delta h_{f_{T_{ref},i}}^o$$

# Examples of enthalpies of formation

Species	$\Delta h_{f,298.15\text{ K}}^{\circ}$ kJ/mol
CO	-110.53
CO <sub>2</sub>	-393.52
CH <sub>4</sub>	-74.87
H	218.00
H <sub>2</sub> O	-241.83
O	249.17
OH	38.99

From NIST-JANAF database 4<sup>th</sup> edition (1998)  
(e.g., [kinetics.nist.gov/janaf](http://kinetics.nist.gov/janaf))

can find newer updates to data

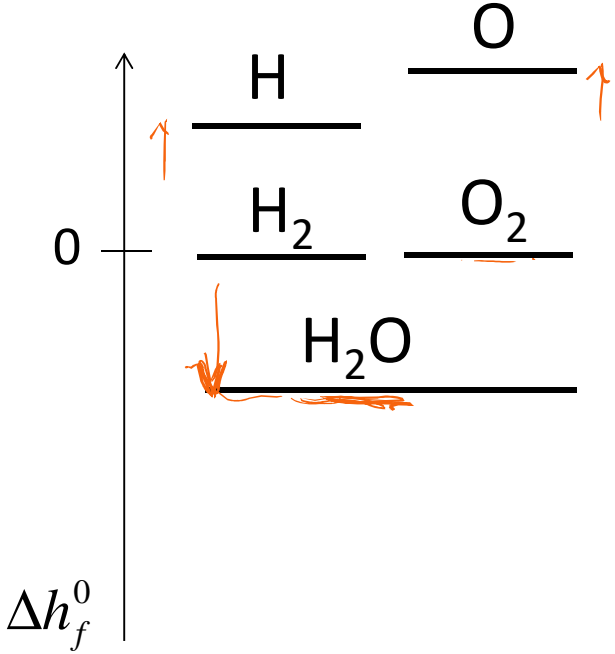
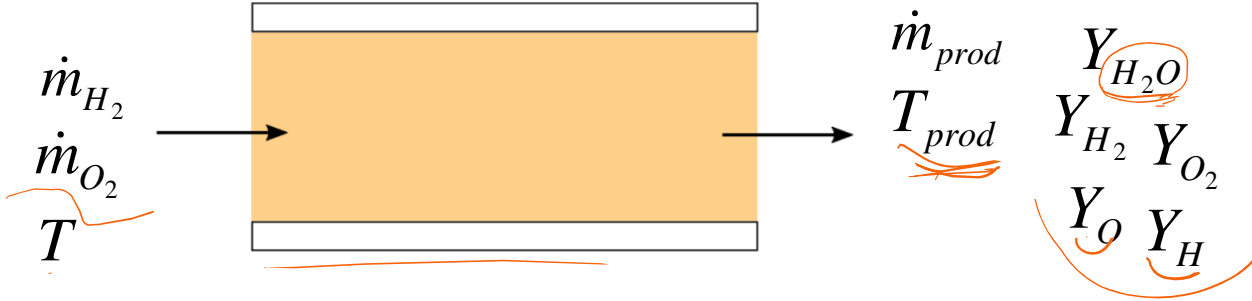
high formation enthalpy species: e.g. H, O

high energy  $\Rightarrow$  hard to make (unstable)

low formation enthalpy species: e.g. CO<sub>2</sub>, H<sub>2</sub>O

low energy ( $\ll 0$ )  $\Rightarrow$  very stable at low T

# Composition influence on temperature

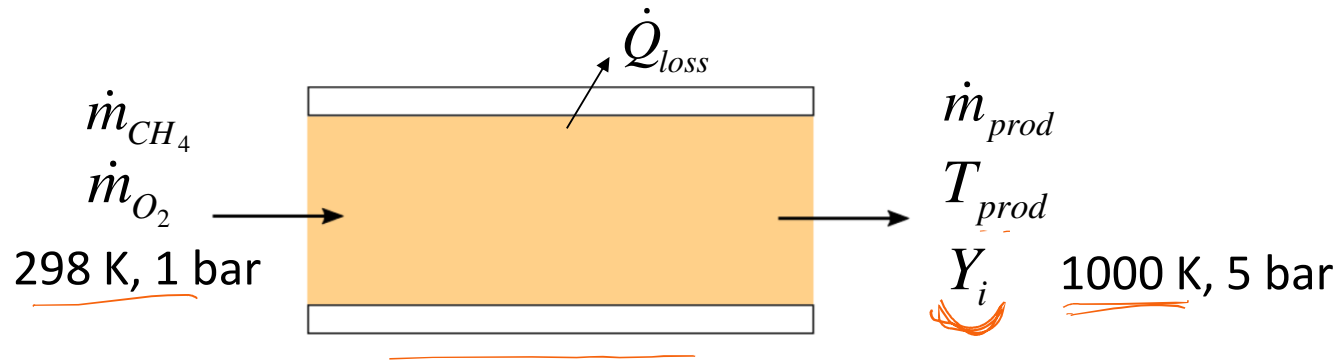


So if the products have more H, O, H<sub>2</sub>, O<sub>2</sub> vs. H<sub>2</sub>O

$T_{prod}$  will be lower than if we could shift them toward water

# Example

## Case of a methane-oxygen combustor



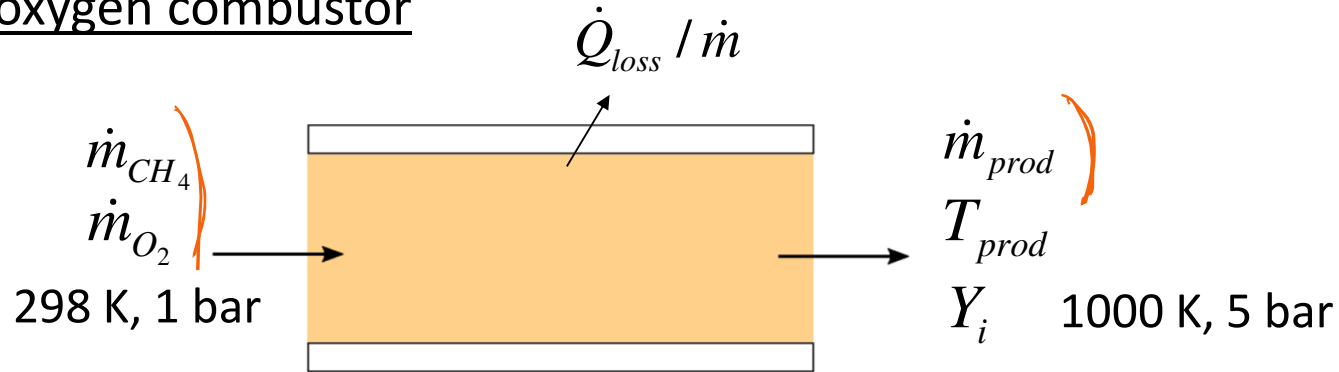
- gaseous methane and oxygen entering non-adiabatic combustor at 298 K, 1 bar (stagnation conditions)
- mass flowrate of oxygen is 5× that for methane
- heat loss results in 1000 K product temperature

Q. what is the heat loss rate per unit mass flow rate,  $\dot{Q}_{loss}/\dot{m}$  ?

assume:  $\frac{\partial \phi}{\partial t} = 0$   $PV = nRT$   $C_p, C_v \neq 0$   
 steady state, no “shaft” work, thermally perfect but not calorically perfect gases

# Example

## Case of a methane-oxygen combustor



### 1. mass conservation

$$\underbrace{\dot{m}_{in}}_{\text{react}} = \underbrace{\dot{m}_{exit}}_{\text{products}} \equiv \dot{m}$$

$$\dot{Q}_{in} - \dot{W}_{shaft} + \int_{CV} \rho \vec{f} \cdot \vec{u} dV - \int_{CS} p(\vec{u} - \vec{u}_{rel}) \cdot \hat{n} dA = \frac{d}{dt} \int_{CV} \rho e_o dV + \int_{CS} \rho h_o (\vec{u}_{rel} \cdot \hat{n}) dA$$

### 2. energy conservation

$$\dot{m} h_{o,in} = \dot{m} h_{o,exit} + \dot{Q}_{loss}$$

$$\dot{Q}_{loss} / \dot{m} = h_{o,in} - h_{o,exit}$$

$$\frac{\dot{Q}_{loss}}{\dot{m}} = h_{o,reactants} - h_{o,products}$$

assume we know molar properties, so use  $h = \bar{h} / MW$

$$= \frac{1}{MW_r} \sum_{\text{reactants}} \chi_i \left[ (\bar{h}_{T_{or}} - \bar{h}_{T_{ref}})_i + \Delta \bar{h}_{f,T_{ref},i}^o \right] - \frac{1}{MW_p} \sum_{\text{products}} \chi_i \left[ (\bar{h}_{T_{op}} - \bar{h}_{T_{ref}})_i + \Delta \bar{h}_{f,T_{ref},i}^o \right]$$